

ENERGY PLANT HOT OIL

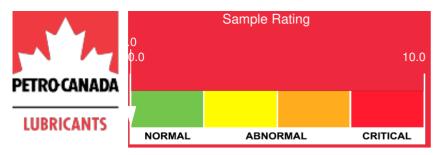
| Customer: PTRHTF20043 | System Information | Sample Information |
|--------------------------------------|----------------------------------|--------------------------|
| WEST FRASER LVI | System Volume: 38000 ltr | Lab No: 02291494 |
| PO BOX 1737 | Bulk Operating Temp: 500F / 260C | Analyst: Gordon Susinski |
| ROCKY MT HOUSE, AB T4T 1B3 | Heating Source: | Sample Date: 06/07/19 |
| Canada | Blanket: | Received Date: 06/17/19 |
| Attn: Renny Ceccato | Fluid: PETRO CANADA PETRO-THERM | Completed: 06/19/19 |
| Tel: | Make: WELLONS | |
| E-Mail: renny.ceccato@westfraser.com | | |

Recommendation: Results are normal

Comments:

| Sample Date | Received Date | Fluid Age | Sample Location | Flash Point (COC) | Water (KF) | Water (KF) Viscosity (40°C) Acid Number | | | GCD 10% | GCD 50% | GCD 90% | GCD % < 335°C |
|-------------|---------------|--|--------------------|-------------------|------------|---|---|----------|----------------------------------|--|---|---------------|
| | mm/dd/yy | | | °F/°C | ppm | cSt | mg/KOH/ g | %wt | °F/°C | °F/°C | °F/°C | % |
| 06/07/19 | 06/17/19 | 1y | HOT OIL PUMP | 410 / 210 | 73.9 | 37.0 | 0.225 | 0.076 | 734 / 390 | 821 / 438 | 915 / 491 | 0.00 |
| 10/26/18 | 11/08/18 | Oy | | 424 / 218 | 151.4 | 37.6 | 0.150 | 0.364 | 728 / 387 | 810 / 432 | 902 / 483 | 0.00 |
| 06/22/18 | 07/04/18 | Oy | PRIMARY PUMP | 439 / 226 | 159.0 | 37.7 | 0.09 | 0.259 | 715 / 379 | 794 / 423 | 899 / 482 | 0.00 |
| 09/15/17 | 10/10/17 | Оy | 72116-4500RB | 403 / 206 | 2467.2 | 57.7 | 0.965 | 1.65 | 700 / 371 | 828 / 442 | 912 / 489 | 3.98 |
| 09/07/17 | 10/10/17 | Oy | 12116-4500RB | 374 / 190 | 51.7 | 57.3 | 1.01 | 0.782 | 734 / 390 | 846 / 452 | 924 / 495 | 3.38 |
| 04/01/17 | 04/12/17 | 12y | PRIMARY PUMP | 370 / 188 | 92.8 | 55.4 | 1.17 | 1.27 | 735 / 391 | 848 / 453 | 932 / 500 | 3.82 |
| 09/09/16 | 09/14/16 | 11y | PRIMARY OIL PUMP | 388 / 198 | 77.1 | 58.6 | 0.949 | 1.65 | 724 / 385 | 844 / 451 | 915 / 491 | 4.35 |
| Acid Number | | Viscosity 60 55 50 50 50 50 50 50 50 50 5 | @ 40°C Sep19/14 | Apri/17- | Sep 15/17 | on an | 240 - 230 - 220 - 210 - 200 - | Mart/1/1 | Apr17/14 Sep 19/14 Feb5/16 | Apr1/17 - Sep 15/17 - Sep 15/1 | 9 3 3 3 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | |

Report ID: [02291494] (Generated: 06/20/2019 09:31:54) - Page 1 - Copyright 2019 Wearcheck Inc. All Rights Reserved.



| Sample Date | Iron | Chromium | Nickel | Aluminum | Copper | Lead | Tin | Cadmium | Silver | Vanadium | Silicon | Sodium | Potassium | Titanium | Molybdenum | Antimony | Manganese | Lithium | Boron | Magnesium | Calcium | Barium | Phosphorus | Zinc |
|----------------------------|---------|-----------------|--------|----------|----------|--------|-----------------|---------|---------|----------|---------|---------|-----------|----------|------------|----------|-----------|---------|-------|-----------|---------|--------|------------|------|
| 06/07/19 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 1 | 0 |
| 10/26/18 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 1 | 0 |
| 06/22/18 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 0 | 2 | 2 |
| 09/15/17 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09/07/17 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04/01/17 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 09/09/16 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| Elen ognte llagnays | sis ges | sul ts (| above | e) ion p | oantos p | benom | illi o n | (pppm) |). [ð0, | 000 p | pm = | 1.9% | 9] 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01/30/15 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 10 | 0 |
| 09/19/14 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 06/20/14 | 16 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 2 |
| 04/17/14 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11/01/13 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 |
| 03/01/13 | 67 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 3 | 0 | 1 | 2 |
| 12/16/11 | 10 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 11 | 0 | 3 | 3 |
| 03/17/11 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 2 |
| 11/26/10 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 |
| 05/14/10 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 2 | 1 |
| | | | | | | | | | His | torica | l Con | nment | S | | | | | | | | | | | |
| | Result | s are n | ormal. | Resan | nple at | the ne | xt inter | val and | contin | ue to m | onitor | the sys | tem. | | | | | | | | | | | |

10/26/18 Calcium levels are higher than expected. Typical sources of this element are other 1.) heat transfer products and 2.) outside contamination. Resample, taking care to obtain a representative sample of the system. Calcium ppm levels are abnormally high. 06/22/18 We are unable to comment on competitive product. Water contamination levels are severely high. Water contamination levels are severely high.. ppm Water contamination levels are severely high. Pentane Insolubles levels are severely high. COC Flash Point is marginally low. 09/15/17 We are unable to comment on competitive product. Pentane Insolubles levels are severely high. COC Flash Point is abnormally low. 09/07/17 determines the amount of con ts in the oil. This value will inc s material. The tur if the fluid o is a measure of the mits. The 90% distil ounds in the oil. e is due to high Ily from ns. Ten 04/01/17 reases the size of the all, the results in the volucions in the oil. This value will increase exponentially once the oxidation process begins. The system that can foul heat exchanger surfaces or plug small lines. The 40°C viscosity is abno The C.O.C. Flash Point is low (188C). This is the lowest temperature at which the fluids vaco urming var rsis results, it appears that the oil may have experienced one or both of the fo anic acids. Oxidation is accelerated by contaminants such as wear debris, du and Oxidation. This may be due in part to the length of servi Changes in the fluid will be seen as discoloration, increased v ons in the oil with oxygen from air, tion of heavy insoluble compounds nds in the oil. Increases in the acid nu ally once the p our if the fluid con ely due to the es to be 09/09/16 is may be due in part to the length of service on the off 1 years indicated. Thermal degradation is the presence of excess heat, the hydrocation molecules teach the breaking point of normally data and to boll before oncellength in the indicated in the service of the service o alysis results, it appears that the oil may have experienced one or both of the follow into lighter hydrocarbons chains. These chains, when formed may have lower vis orbonaceous material by baking it on the tubes and then act as an insulation layer, between oxygen and the components of the oil whereby the hydrocarbon in the ce-nsfer system, the most probable place for fluid oxidation to occur is in the expansio of service, this system may be due for an oil charge? Resample at the next inter sities, lower flash points and start to boil before normal fresh oil would thus, affecting the rhese carbonaceous layers can flake away and produce hot spots on the tubes possibly r 02/05/16 e hydrocarbon in the oil turns into weak carboxylic acid occur is in the expansion tank (without an inert gas blan ample at the next interval and continue to monitor the s a closed heat transfer system, the oil.After 11 years of service, this sy

01/30/15

This sample is thoring signs of hermal departations as well as signs of oxidation. The flash point is very low and the system needs to be vented immediately in order to bleed off the light ends from the system. This should help raise the flashpoint. After system has been vented, re-sample and send in for analysis. Pertane insolubles levels are serverive hiol. Cover

06/20/14

The oil condition remains concerning, therefore we are writing the same comments form the last sample in June. The oil is showing increased signs of degradation by oxidation with the TAN increasing to very high level. Solids content is also high. This system has shown degradation for a couple years at least and we suggest that if budget permits and if productivity is starting to be affected, that a system cleaning shoud be considered. If this is too costly and productivity has not been affected, maybe a drain and refill to remove this heavily degraded oil out of the system is a more cost effective solution that will bring value and delay a full system cleaning by a few more years. Keep running the system with this fluid degrading further will get to a point where it will require a costly cleaning and associated downtime. Pentane Insolubles levels are severely high. Acid Number (AN) is severely high. COC Flash Point is abnormally low. (GCD) 90% Distillation Point is marginally high.

04/17/14

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11/01/13

The distillation data has not changed much since the last sample. There is a significant increase in the acid number (AN) as well as the solids but other parameters not showing a concern. Very slight increase in the viscosity although would expect higher with TAN and Solids. Recommend to re-sample in 6 months. Pentane Insolubles levels are severely high. Acid Number (AN) is severely high. COC Flash Point is severely low. (GCD) 10% Distillation Point is abnormally low. (GCD) % < 335°C is marginally high. (GCD) 90% Distillation Point is marginally high.

03/01/13

The overall condition of the oil is not so bad. The amount of solids appears to be rising. The flash point decreased but this is strange considering the boiling curve (GCD) data indicate the amount of light hydrocarbons present in the oil dropped, which should have increased the flash point. The Acid NUmber dropped which is good news. Pentane Insolubles levels are severely high. COC Flash Point is severely low.

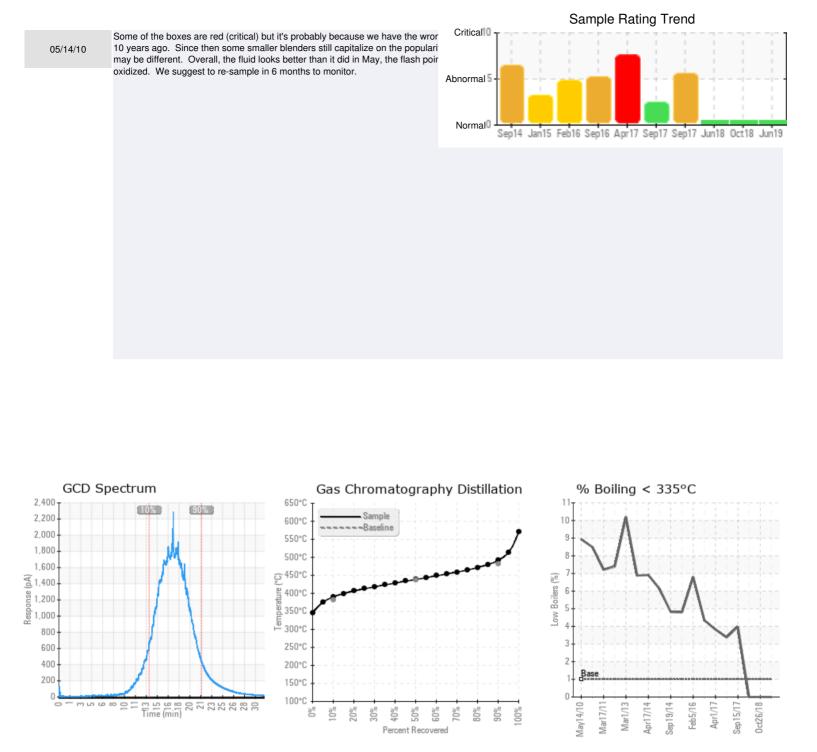
12/16/11

The flash point of this oil is low considering its high viscosity. Since the only benefit of having a high viscosity oil is normally its high flash point, in this case the flash point is even lower than most heat transfer fluids. The oxidation (degradation) level of the oil is roughly the same since the last sample, except the amount of solids in the oil is very high. Pentane Insolubles levels are severely high. Acid Number (AN) is abnormally high. COC Flash Point is marginally low.

03/17/11

The fluid seems to suffer from both thermal degradation and oxidation. Oxidation is noticeable by the high Total Acid Number. The thermal cracking is evident by looking ast the reduced flash point and lower GCD 10% (begining of the boiling curve of the fluid). The fluid is more volatile than fresh oil because thermal cracking formed low boiling point hydrocarbons ("low boilers") which represent 7% of the system currently. We strongly suggest to plan for action on this system, whether it's sweetening (partial drain&add fresh oil) or something to try to improve the fluid quality and run for a couple more years before having to do a complete clean-flush-refill of this system.

The condition of the Sun HT 21 has not changed much since the last sample. Flash point looks acceptable considering the operating temperature. Re-sample at next regular sampling interval



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The oil is either mixed with a lighter viscosity oil or has suffered thermal degradation. 8.9% by weight of the sample are low boilers that are not generally found in fresh oil. On the oxidation side, the Acid Number is moderately high at 0.36 mg KOH/g. In large systems this would be considered very high because of the large amount of oil that has oxidized to reach this level.